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DETERMINATION OF POLYMER MOLECULAR WEIGHT AND MOLECULAR WEIGHT DISTRIBUTION BY REVERSE PHASE THIN LAYER CHROMATOGRAPHY

K. H. Bui and D. W. Armstrong*

Department of Chemistry Texas Tech University Lubbock, Texas 79409

ABSTRACT

Reverse phase thin layer chromatography (RPTLC) and scanning densitometry was used to determine various molecular weight averages and the molecular weight distribution of broad molecular weight range samples of poly(styrene) and poly(methyl metharcylate). A basic program was developed which analyzes the analog signals from the scanner, calculates the desired parameters, prints the parameters, graphs the results and simultaneously displays the results on a CRT. The average molecular weight values obtained by this technique compare well to those obtained by other methods.

INTRODUCTION

The ability of RPTLC to efficiently fractionate a variety of synthetic polymers using a binary solvent mobile phase consisting of a thermodynamically "good" solvent and a thermodynamically "poor" solvent of the polymer was recently reported (1-3). The mechanism of fractionation was demonstrated to be a selective

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precipitation of the polymer resulting from the continuous change in mobile phase composition during development (1,2,4). In RPTLC the depletion of the less polar "good" solvent can occur naturally via selective absorption (during development) by the nonpolar stationary phase.

In addition to its high resolving power, RPTLC has several other advantages over conventional normal phase TLC methods for the separation of polymers. It is applicable to a greater variety of polymers as well as to a greater molecular weight range (2,5). In this work the applicability of RPTLC for the analysis of polymer molecular weights and polydispersity is evaluated.

MATERIALS

Whatman KC18F reversed phase TLC plates (5 x 20 cm and 20 x 20 cm) were used in all fractionations. HPLC grade methanol, methylene chloride, tetrahydrofuran (from Waters Associate), ethylene glycol (from Sigma Co.) and resublimed iodine (from Fisher Scientific Co.) were used as received. The polymer standards, their manufacturers and the various average molecular weight values supplied by the manufacturer are listed in Table I.

METHODS

All polymer standards were dissolved in methylene chloride (5 mg/ml) and 2 μ l of the solution was deposited on the TLC plates via a Drummond 5 μ l micropipette. All TLC fractionations were done in an 11 3/4 in. long, 4 in. wide and 10 3/4 in. high Chromaflex developing chamber. Both the narrow molecular weight range

TABLE I

Polymers Standards. The Average Molecular Weights are Certified by the Indicated Suppliers

Polymers	MW	Mw	Mn	Mw/Mn	Suppliers
Polv(stvrene)	_	257800	<u> </u>	2.1	NBS*
	-	37400	35800	1.04	NBS*
	900000	929000	850000	1.09	Polv Science
	233000	254000	217600	1.17	Poly Science
	100000	93050	926000	1.04	Poly Science
	100000	-	-	1.3	Poly Science
	3700000	~	-	1.2	Waters
	390000		-	1.04	Waters
	110000		-	1.1	Waters
	35000	-	-	1.04	Waters
	17500	-	-	1.04	Waters
Polv(methvl					
methacrvlate)	_	81000	47000	1.7	Polv Science
	45000	-	-	1.09	Polymer
					Laboratories
	72000		-	1.08	Polymer
					Laboratories
	96000	-	-	1.10	Polymer
					Laboratories
	280000	~	-	1.15	Polymer
					Laboratories
	48000	~	-	1.16	Polymer
					Laboratories
	64000	~	-	1.16	Polvmer
					Laboratories

*National Bureau of Standards

standards and the broad molecular weight range polymer (used as the unknown) were spotted on the same plate and the calibration curve was established using the elution data of the narrow molecular weight range standards. Typical calibration curves for poly(styrene) and poly(methyl methacrylate) are shown in Figure I.



Figure 1. Typical TLC calibration curves for poly(styrene) developed with a 77.5:22.5 (v:v) MeCl₂:MeOH mobile phase (●) and with a 79:21 (v:v) MeCl₂:MeOH mobile phase (□). The poly(methyl methacrylate) calibration curves were obtained using a 76:24 (v:v) THF:ethylene glycol mobil phase (●) and a 39:61 (v:v) MeCl₂:MeOH mobil phase (△).

It is apparent that for both polymer systems, there is a linear relationship between the R_f values (or elution distance) and the log of their molecular weight. Furthermore, this relationship holds for different mobile phase compositions and mobile phase systems. Consequently calibration can be done simply by linearly

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correlating the molecular weight of the polymers to their elution Quantitative analysis of the polymer concentration along values. its elution path was performed via direct scanning densitometry using a Shimadzu model CS 910 dual wavelength TLC scanner. For polystyrene, maximum absorption occurs at wavelength of around 265 nm and almost no absorption occurs at 300 nm. Therefore, the sample wavelength was set at 265 nm and the reference wavelength was set at 300 nm. Detection was performed in the reflectance mode (Figure 3). Unusually high noise levels and baselines were observed (even under dual wavelength scan) when the KC 18 plates were scanned at 265 nm. This phenomenon is believed to be caused by the presence of the fluorescence indicator which has emission bands that extend into the UV. In the analysis of polydispersity of a polymer, this unusually high baseline is very deleterious since only the top portion of the peak (which protrudes above the base line) can be detected and the peak and hence the polydispersity of the polymer will appear to be artificially very narrow. Fortunately, the fluorescence indicator can be easily destroyed by spraying the plate with an 8% sulfuric acid/ethanol solution and heating the plate at 100°C for 10 minutes. Figure 2 shows that both the noise level and the baseline were considerably improved when the above treatment was performed on part of the plate. Consequently, the sensitivity of the detection is also enhanced with this treatment (Figure 3).

In order to visualize poly(methyl methacrylate), a 1% methanolic iodine solution was sprayed on the plate. After warming the plate at \sim 50°C for a few minutes and letting the yellow background



PLATE LENGTH, CM

Figure 2: Scanning densitometric profile of a reversed phase TLC plate with fluorescent indicator. Part "A" of the plate was sprayed with H₂SO₄/EtOH solution and Part "B" was untreated. Note that the baseline is lower and more stable when the fluorescent indicator has been inactivated. The magnitude of this effect is dependent on the scanning wavelength used.



- - ○, = reflectance mode without treatment of plate
 - ▲, ▲ = transmission mode without treatment of plate

of the plate fade, poly(methyl methacrylates) appeared as yellowbrown spots. The maximum absorption of these spots occured at 405 nm. Scanning densitometry of these spots, performed under single wavelength transmission mode provided the highest sensitivity (see Figure 4).

A Shimadzu Chromatopac model CR2A(X) data processor was used to analyze the analog data collected from the TLC scanner. The Chromatopac can function as a data processor as well as a per-



Figure 4: Plots of the weight of poly(methyl methacrylate) spotted on a TLC plate versus densitometric peak area. The circles (O) are for quantitation done in the transmission mode and the squares (D) are for quantitation of the same spots in the reflectance mode. The scanning wavelength was 405 nm (after spraying with iodine solution).

sonal computer. Data processed by the chromatopac such as peak retention time, peak area, area of a certain time band (slice area), retention time of the slice area, etc. can be manipulated freely as variables by a user defined Basic program. A Basic program was developed which permits calculations of the various average molecular weights and the polydispersity as well as the graphical display of the cumulative weight fraction molecular weight distribution and the weight fraction frequency distribution of the polymers. A listing of the program is provided in Appendix I.

RESULTS AND DISCUSSION

Figure 5 illustrates the scanning densitometric profile of a TLC chromatogram showing the fractionation of a mixture of 4 narrow disperse poly(styrene) standards and of a broad molecular weight range poly(styrene) standard (please note that these standards and standard mixtures were spotted on the same plate and developed under identical conditions). These scanning densitometric profiles are essentially a molecular weight size distribution of the polymer in weight concentration if and only if a detection method which is sensitive only to the weight concentration of the polymer and not the molecular weight of the polymer is used. Light absorption of polymers has been shown to be independent of the polymer molecular weight and to vary linearly with the concentration of the polymer in different solvent systems (when in sufficiently dilute solution) (6,7). Indeed Figure 3 shows that the UV absorption of poly(styrene) is independent of its molecular

52



Figure 5: Two superimposed scanning densitometric profiles of a poly(styrene) unknown (i.e., the solid line, ---) and poly(styrene) standards (i.e., the broken line, ---). Above the profiles is the calibration curve for the standards (i.e., log MW vs. elution distance).

weight and varies linearly with the concentration of the polymer (up to $\sim 15 \ \mu$ g). Using the scanning densitometric profile of the mixture of narrow disperse standards, a calibration curve can be readily established. From this calibration curve, the scanning densitometric profile of the broad molecular weight range standard is converted into a molecular weight distribution curve and the respective molecular weight averages can be calculated (i.e., including number average, weight average and z-average molecular weights. See Appendix I).

The various molecular weight averages of broad distribution poly(styrene) and poly(methyl methacrylate) standards determined

TABLE	II.
-------	-----

A Comparison of Polymer Molecular Weight Averages Obtained by RPTLC and Other Traditional Methods

Polystyrene ⁽¹⁾ (NBS)	Average Mw by RPTLC	Stand ar d Deviation	Average MW given by Manufacturer
Mw	2.45 x 10 ⁴	9 0 00	2.58 x 10 ⁴ (light scat- tering) 2.88 x 10 ⁴ (sedimentation equilibrium)
Mn	1.20×10^4	9000	1.23 (fractionation) $*$
Mw/Mn	2.0	-	2.1
Polymethyl Methacrylate(2) (Poly Sciences)			
Mw	8.0×10^4	3000	8.1 x 10 ⁴ (light scat- tering)
Mn	5.4 x 10^4	3000	4.7 x 10^4 (osmometry)
Mw/Mn	1.5		1.7

*Based on fractionation value of Mw/Mn multiplied by Mn value for light scattering

- (1) Fractionated using 78:22 (v:v) MeCl₂/MeOH. Sample loading = 5 mg/ml. Analyzed in the reflectance mode at 265 nm after spraying with ethanolic sulfuric acid solution.
- (2) Fractionated using 30:70 (v:v) (MeCl₂/MeOH). Sample loading = 5 mg/ml. Analyzed in the transmission mode at 405 nm after spraying with methanolic iodine solution.

TABLE III.

Polymers	Solvent Pairs	Reference
Poly(styrene)	MeCl ₂ /MeOH	1
Poly(a-styrene)	MeCl ₂ /MeOH	2
Poly(methyl methacrylate)	MeCl ₂ /MeOH [*] ; THF:EG	2
Poly(ethylene glycol)	Dioxan/Ethylene glycol; MeOH/EG	2
Poly(ethylene oxide)	Dioxan/EG	2
Poly(vinyl chloride	THF:EG	8
Poly(vinyl acetate)	THF:EG	8
Poly(isoprene)	MeCl ₂ /MeOH	2
Poly(butadiene)	MeCl ₂ /MeOH	2
Poly(tetrahydrofuran)	THF:EG	2

Polymers Which Have Been Fractionated by RPTLC

* This work

by this technique are compared to those given by the manufacturers in Table II. It is apparent that the average molecular weight values determined by this technique compare well to those given by the manufacturers in spite of the fact that no correction for band broadening due to processes other than the fractionation process was made (in TLC fractionation of polymer, band broadening can be caused not only by the polydispersity of the polymer but also by other processes such as eddy diffusion and mass transfer).

Table III lists all the polymers which have been fractionated by RPTLC and the solvent pairs used to fractionate them. It is apparent that except for those polymers which exist in the crystalline state (where elevated temperature is needed to break up the crystalline bond forces before dissolution of these polymers can occur) this technique is readily applicable to the analysis of a variety of macromolecules.

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APPENDIX I

LIST BASIC PROGRAM

5 PRINT " *** MOLECULAR WEIGHT REPORT ***" 6 P.:P. 18 PRINT "CALIBRATION DATA" 20 PRINT "COEFFICIENT A";:INPUT A

56

```
PRINT "COEFFICIENT B"J: INPUT B
30
       PRINT "COEFFICIENT C"J:INPUT C
411
       PRINT "COEFFICIENT D"F:INPUT D
50
       P=MAXSL(1)
бĤ
70
       DIM AR(P),M(P),L(P),CU(P)
       T=0:X=0:Y=0:ZA=0:ZB=0:ZC=0:AM=0
100
120
       FOR J=1 TO P
       T=T+SLAR(1,J)
130
140
        NÉXT J
145
       PRINT
                      ";"Slice ";"Mol.Wt ";"Area ";"Cum"
";" Area ";" Slice ";" % ";"AR."
       PRINT "Ret.
150
       PRINT "Time "J" Area "J" Slice "J"
PRINT "_____"
155
156
157
        PRINT
160
       FOR I=1 TO P
       M(I)=A+B#SLRT(1,I)+C#SLRT(1,I)^2+B#SLRT(1,I)^3
170
175
       L(I)=10^M(I)
180
       AR(I)=100#SLAR(1,I)/T
185
       IF AM(AR(I) THEN AM=AR(I)
190
        X=X+SLAR(1,I)
200
        Y=Y+SLAR(1,I)/L(I)
210
        ZA=ZA+SLAR(1,I)*L(1)
220
        ZB=ZB+SLAR(1)I)#(L(1)^2)
530
        ZC=ZC+SLAR(1,I)*L(I)^3
250
       CU(I)=100*X/T
898
       PRINT USING 261; SERT(1,1), SLAR(1,1), L(1), AR(1), CU(1)
       IMAGE; ##. ## ####. # ######### ##.# ##.#
261
270
        NEXT I
280
       MW=ZA/X
290
       MN=X/Y
300
       MA=ZB/ZA
310
       MB=ZC/ZB
       MP=MW/MN
315
       P.:P.:P.
316
       PRINT "Distribution Averages:"
317
318
       PRINT "Total Area =",T
       PRINT "Mn =",MN
320
       PRINT "Mw =",MW
325
       PRINT "Mz =",MA
330
340
       PRINT "MZ+1 =",MB
       PRINT "MW/MN =", MP
350
355
       P.:P.:P.
       PRINT "Range of Log MW Plotted?"
370
       PRINT "Minimum Log MW value";:INPUT MI
PRINT "Maximum Log MW value";:INPUT MX
380
390
392
       P.:P.:P.
       PRINT "4"
393
395
       PRINT
                                                   AREA %"
396
       PRINT
490
       Q=MX-MI
       PVL=0
410
       MOVE PRINTER,0,0
MOVE CRT 400,10
420
440
       MOVE PRINTER, 900,0
445
       PRINT USING 447;AM
446
447
        IMAGE##.##
       MOVE CRT 70,20
448
449
        DRAN CRT 450,20
450
       MOVE PRINTER, 120, 100
        DRAM PRINTER, 920, 100
455
        FOR I=10 TO 0 STEP -1
456
        MOVE PRINTER, 80*1+120, 100
457
        DRAW PRINTER, 80#1+120, 140
458
        MOVE CRT 38#1+70,24
DRAH CRT 38#1+70,20
459
460
        NEXT I
461
```

462	DRAW CRT 70,180
463	DRAW CRT 450,180
469	DRAW PRINTER 120,2300
479	DRÁN PRINTER,920,2300
472	FOR I=10 TO 0 STEP -2
474	MOVE CRT 38#I+70,180
475	DRAH CRT 38#1+70,176
47.6	MOVE PRINTER,80#I+120,2300
477	DRAW PRINTER,80#I+120,2260
478	NEXT I
480	MOVE PRINTER,920,2300
481	DRAW PRINTER, 920, 100
482	MOVE CRT 450,180
483	DRAW CRT 450,20
500	FOR I=0 TO Q
510	MOVE PRINTER, 50, (2200#1/0)+100
512	MOVE CRT 30, (160#1/0)+20
520	PRINT USING 530; MX-I
530	(MAGE:+
540	MOVE PRINTER, 120, (2200#1/Q)+100
550	DRAW PRINTER, 130, (2200#1/Q)+100
551	MOVE CRT 70, (160*1/0)+20
552	DRAW CRT 75, (160#1/0)+20
554	MOVE PRINTER, 910, (2200#1/0)+100
555	DRAW PRINTER, 920, (2200#1/Q)+100
556	MOVE CRT 445, (160*1/0)+20
557	DRAW CRT 450,(160*1/Q)+20
569	NFXT I
659	MOVE PRINTER, 120, (2200*(MX-M(1))/0)+100
651	MOVE CRT 70,160*(MX-M(1))/0+20
660	FOR I=1 TO P
679	DRAW PRINTER, 8*CU(I)+120, 2200*(MX-M(I))/0+100
671	0RAW CRT 3.8*CU(I)+70,160*(MX-M(I))/0+20
699	NFXT I
695	MOVE PRINTER, 120, 2200*(MX-M(1))/0+100
696	MOVE CRT 70,160*(MX-M(1))/0+20
788	FOR I=1 TO P
219	DRAW PRINTER, 800*AR(I)/AN+120,2200*(MX-M(I))/Q+100
211	0RAU CRT 380#AR(1)/AM+70+160#(MX-M(1))/Q+20
728	NEXT 1
230	MOVE PRINTER, 0, 2400
731	MOVE CRT 0-190
749	P. USING 750; "105 MW", "0", "20", "40", "60"
758	
760	MAVE PRINTER, 728, 2488
265	MOVE CRT 350,190
779	PRINT " 80 100"
225	PRINT
780	PRINT " CUM APPA 7"
300	END